



NATIONAL CERTIFIED TESTING LABORATORIES

FIVE LEIGH DRIVE • YORK, PENNSYLVANIA 17406 • TELEPHONE (717) 846-1200
FAX (717) 767-4100
www.nctlinc.com

PRODUCT APPROVAL SUPPORTING CALCULATIONS

F-4500 Inswing and Outswing Doors (non-Impact)

REPORT TO:

**JELD-WEN WINDOWS & DOORS
3737 LAKEPORT BLVD
KLAMATH FALLS, OREGON**

REPORT NUMBER: NCTL-110-26137-1
REPORT DATE: 04/02/23

Joseph A. Reed, PE
FL PE 58920
FL REG 33474

This item has been digitally signed and sealed by Joseph A. Reed, PE on the date adjacent to the seal.

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Scope

National Certified Testing Laboratories was contracted by Jeld-Wen Windows & Doors to evaluate alternate installation methods for their F-4500 Inswing and Outswing Doors (non-Impact). The evaluation is based on physical testing and product certifications. Reference standards utilized in this project include:

Florida Building Code, Building. International Code Council.

ANSI/AWC National Design Specification (NDS) for Wood Construction. American Wood Council.

AISI S100 North American Specification for the Design of Cold-Formed Steel Structural Members. American Iron and Steel Institute.

ICC-ES Report ESR-1976 ITW Buildex TEKS Self-Drilling Fasteners. ICC Evaluation Service.

NOA 21-0201.06 Tapcon Concrete and Masonry Anchors with Advanced Threadform Technology. Miami-Dade County Product Control Section.

The anchorage analyses presented herein do not address the water resistance, water penetration or air infiltration performance of the installation method or the installed product. In addition, the analyses rely on the assumption that the building substrate is capable of withstanding incurred loads.

Certification of Independence

In accordance with Rule 61G20-3 Florida Administrative Code, National Certified Testing Laboratories hereby certifies the following:

- National Certified Testing Laboratories does not have, nor does it intend to acquire or will it acquire, a financial interest in any company manufacturing or distributing products tested or labeled by the agency.
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Analyses

Summary of Test Results

The following table summarizes the various F-4500 Inswing and Outswing Doors (non-Impact) products and their corresponding performance levels which have been established by testing or product certification.

Table 1 Summary of Test Results

Series/Model	Test Report Number	Size (W x H)	Performance
F-4500 Inswing Door (XX) Through Frame Install	NCTL-310-22-108 (Rev. 2, 03/02/23)	72" x 79"	+50/-55 psf
F-4500 Outswing Door (XX) Through Frame Install	NCTL-310-23-002 (Rev. 4, 03/14/23)	72" x 78"	+50/-55 psf

Testing documented in Table 1 was conducted by National Certified Testing Laboratories in Everett, Washington (Florida Department of Business & Professional Regulation Test Lab No. TST9341, A2LA Laboratory Certificate 3054.03).

As-Tested Installation Analysis

For air/water/structural testing the test specimen was secured to a 2x Spruce-Pine-Fir buck. The as-tested installation method is evaluated on page 3 to page 5. These capacities will be used to prove acceptable alternate anchors and substrates for the product.

Alternate Anchorages

Calculations on page 6 through page 15 determine the design capacity of alternate installation anchorages for the product.

Anchorage Requirements

As-tested spacing must be maintained. It must be determined the anchorages are not overloaded for the approved product size and design pressures. Calculations presented on page 16 show the alternate anchorages are acceptable for the established product performance.

Anchorage requirements established by this report are accurately presented in Drawing D1000255.

Attachments

Appendix A – Revision Log (1 page)



As-Tested Installation – Through Frame to Wood

#8 Flat Head Screw; 1-1/2" penetration to wood

3/4" thick Wood Frame (G = 0.42)

1/4" Maximum Shim Space

Spruce-Pine-Fir 2x Wood Substrate Minimum (G=0.42)

Allowable Shear of #8 Flat Head Screw

Z' = 110 lb (See Following 2 Pages)

Bending of #8 Flat Head Screw

L = 1/4" (maximum shim space)

$S = \pi d^3/32 = \pi(0.131)^3/32 = 0.000221 \text{ in}^3$

$F_b = (1.3)(0.6F_y) = (1.3)(0.6)(90,000 \text{ psi}) = 70,200 \text{ psi}$ (1.3 weak axis factor)

$F_b = M/S = (VL/2)/S$ (L/2 for guided bending)

$V = 2SF_b/L = (2)(0.000221 \text{ in}^3)(70,200 \text{ psi})/0.25" = 124 \text{ lb.}$

Capacity of Connection is 110 lb



As-Tested Installation – Through Frame to Wood (Continued)

Lateral Design Strength of Wood Connections

Data

Fastener			
Fastener	=	#8 Wood Screw	
Shank Dia	=	0.164	in.
Root Dia.	=	0.131	in.
F_{yb}	=	90,000	psi
Fastener length	=	2.000	in.

Main Member			
Material	=	SPF	
G	=	0.42	
θ	=	90	\leq (Angle of load to grain $0^\circ \leq \theta \leq 90^\circ$)
F_e	=	3,350	psi
Thickness	=	1.500	in.

Side Member			
Material	=	SPF	
G	=	0.42	
θ	=	90	\leq (Angle of load to grain $0^\circ \leq \theta \leq 90^\circ$)
F_{es}	=	3,350	psi
Thickness	=	0.750	in.

Calculations

Lateral Bearing Factors			
D	=	0.131	in.
ℓ_m	=	0.922	in.
K_θ	=	1.25	
K_D	=	2.20	
R_e	=	1.000	
R_t	=	1.23	
k_1	=	0.4659	
k_2	=	1.2549	
k_3	=	1.37	



As-Tested Installation – Through Frame to Wood (Continued)

Yield Mode	R _d
I _m , I _s	2.20
II	2.20
III _m , III _s , IV	2.20

Lateral Design Values, Z

Mode I _m	=	184	lbf
Mode I _s	=	150	lbf
Mode II	=	70	lbf
Mode III _m	=	77	lbf
Mode III _s	=	69	lbf
Mode IV	=	78	lbf
C _D	=	1.6	

<===== Minimum Value

Wet Service Factor

Fabrication/In-Service	Dry/Dry
C _M	= 1.0
In service temperature	T ≤ 100°F
C _t	= 1.0
C _g	= 1.0
C _Δ	= 1.0
Is fastener installed in end grain?	No
C _{eg}	= 1.00
Is fastener part of a diaphragm?	No
C _{di}	= 1.0
Is fastener toe-nailed?	No
C _{tn}	= 1.00
Z'	= 110 lbf



Alternate Installation – Strap Anchor to Wood

#8 x 1-1/2" Flat Head Screw securing strap to substrate

Spruce-Pine-Fir 2x Wood Substrate Minimum (G=0.42)

Two #8 Screws securing strap to frame

3/4" thick Wood Frame

20 gauge (0.033" thick) 33 KSI Steel Strap Anchor

1/4" Maximum Shim Space

Allowable Shear of #8 x 1-1/2" Flat Head Screw

$$Z' = 122 \text{ lb} \quad (\text{See Following 2 Pages})$$

Bending of #8 x 1-1/2" Flat Head Screw

$$L = 1/4" \text{ (maximum shim space)}$$

$$S = \pi d^3/32 = \pi(0.131)^3/32 = 0.000221 \text{ in}^3$$

$$F_b = (1.3)(0.6F_y) = (1.3)(0.6)(90,000 \text{ psi}) = 70,200 \text{ psi} \text{ (1.3 weak axis factor)}$$

$$F_b = M/S = (VL/2)/S \text{ (L/2 for guided bending)}$$

$$V = 2SF_b/L = (2)(0.000221 \text{ in}^3)(70,200 \text{ psi})/0.25" = 124 \text{ lb.}$$

Bearing of #8 Screw on Frame

$$V_a = F_eDt/K_D = (3,350 \text{ psi})(0.164")(0.75")/(10(0.164)+0.5) = 193 \text{ lb}$$

Bearing of #8 Screw on Strap Anchor

$$V_a = 2.7DtF_{tw}/3.0$$

$$V_a = 2.7(0.164")(0.033")(45,000 \text{ psi})/3.0$$

$$V_a = 219 \text{ lb.}$$

Capacity of Connection is 122 lb



Alternate Installation – Strap Anchor to Wood (Continued)

Lateral Design Strength of Wood Connections

Data

Fastener	
Fastener	= #8 Wood Screw
Shank Dia	= 0.164 in.
Root Dia.	= 0.131 in.
F _{yb}	= 90,000 psi
Fastener length	= 2.500 in.
Main Member	
Material	= SPF
G	= 0.42
θ	= 90 ≤ (Angle of load to grain 0° ≤ θ ≤ 90°)
F _e	= 3,350 psi
Thickness	= 1.500 in.
Side Member	
Material	= ASTM A 653, Grade 33 Steel
G	= N/A
θ	= 90 ≤ (Angle of load to grain 0° ≤ θ ≤ 90°)
F _{es}	= 61,850 psi
Thickness	= 0.033 in.

Calculations

Lateral Bearing Factors

D	=	0.131	in.
ℓ _m	=	1.500	in.
K _θ	=	1.25	
K _D	=	2.20	
R _e	=	0.054	
R _t	=	45.45	
k ₁	=	1.0041	
k ₂	=	0.5032	
k ₃	=	23.87	

Yield Mode	R _d
I _m , I _s	2.20
II	2.20
III _m , III _s , IV	2.20



Alternate Installation – Strap Anchor to Wood (Continued)

Lateral Design Values, Z

Mode I _m	=	299	lbf
Mode I _s	=	122	lbf
Mode II	=	122	lbf
Mode III _m	=	136	lbf
Mode III _s	=	77	lbf
Mode IV	=	108	lbf
C _D	=	1.6	

<===== Minimum Value

Wet Service Factor

Fabrication/In-Service	Dry/Dry
C _M	= 1.0
In service temperature	T ≤ 100°F
C _t	= 1.0
C _g	= 1.0
C _Δ	= 1.0
Is fastener installed in end grain?	No
C _{eg}	= 1.00
Is fastener part of a diaphragm?	No
C _{di}	= 1.0
Is fastener toe-nailed?	No
C _{tn}	= 1.00
Z'	= <u>122</u> lbf



Alternate Installation – Through Frame to Concrete

3/16" Tapcon Anchor

2-1/2" Minimum Edge Distance, 1-1/4" Minimum Embedment

1/4" Maximum Shim Space

Minimum $f'_c = 3,000$ psi Concrete

Allowable Shear of 3/16" Tapcon Anchor

$$P_{ss}/\Omega = 181 \text{ lb} \quad (\text{NOA 21-0201.06})$$

Bearing of 3/16" Tapcon Anchor on Frame

$$V_a = F_e D t / K_D = (3,350 \text{ psi})(0.170")(0.75") / (10(0.170) + 0.5) = 194 \text{ lb}$$

Bending of 3/16" Tapcon Anchor

$$L = 1/4" \text{ (Maximum Shim Space)}$$

$$S = \pi d^3 / 32 = \pi (0.170")^3 / 32 = 0.000482 \text{ in}^3$$

$$F_b = (1.3)(0.6F_y) = (1.3)(0.6)(137,000 \text{ psi}) = 106,860 \text{ psi} \text{ (1.3 weak axis factor)}$$

$$F_b = M/S = (VL/2)/S \text{ (L/2 for guided bending)}$$

$$V = 2SF_b/L = (2)(0.000482 \text{ in}^3)(106,860 \text{ psi})/0.25" = 412 \text{ lb.}$$

Capacity of Connection is 181 lb



Alternate Installation – Through Frame to CMU

3/16" Tapcon Anchor

2-1/2" Minimum Edge Distance, 1-1/4" Minimum Embedment

1/4" Maximum Shim Space

Minimum ASTM C90 Concrete Masonry Unit

Allowable Shear of 3/16" Tapcon Anchor

$$P_{ss}/\Omega = 135 \text{ lb} \quad (\text{NOA 21-0201.06})$$

Bearing of 3/16" Tapcon Anchor on Frame

$$V_a = F_e D t / K_D = (3,350 \text{ psi})(0.170")(0.75") / (10(0.170) + 0.5) = 194 \text{ lb}$$

Bending of 3/16" Tapcon Anchor

$$L = 1/4" \text{ (Maximum Shim Space)}$$

$$S = \pi d^3 / 32 = \pi (0.170")^3 / 32 = 0.000482 \text{ in}^3$$

$$F_b = (1.3)(0.6F_y) = (1.3)(0.6)(137,000 \text{ psi}) = 106,860 \text{ psi} \text{ (1.3 for weak axis bending)}$$

$$F_b = M/S = (VL/2)/S \text{ (L/2 for guided bending)}$$

$$V = 2SF_b/L = (2)(0.000482 \text{ in}^3)(106,860 \text{ psi})/0.25" = 412 \text{ lb.}$$

Capacity of Connection is 135 lb



Alternate Installation – Strap Anchor to Concrete

3/16" Tapcon Anchor; 2-1/2" Minimum Edge Distance, 1-1/4" Minimum Embedment

#8 Screws Connecting Strap to Frame

3/4" thick Wood Frame

20 gauge (0.033" thick) 33 KSI Steel Strap Anchor

1/4" Maximum Shim Space

Minimum $f'_c = 3,000$ psi Concrete

Allowable Shear of 3/16" Tapcon Anchor

$$P_{ss}/\Omega = 181 \text{ lb} \quad (\text{NOA 21-0201.06})$$

Bearing of 3/16" Tapcon Anchor on Strap Anchor

$$V_a = 2.7DtF_{tu}/3.0$$

$$V_a = 2.7(0.170")(0.033")(45,000 \text{ psi})/3.0$$

$$V_a = 227 \text{ lb.}$$

Bending of 3/16" Tapcon Anchor

$$L = 1/4" \text{ (Maximum Shim Space)}$$

$$S = \pi d^3/32 = \pi(0.170")^3/32 = 0.000482 \text{ in}^3$$

$$F_b = (1.3)(0.6F_y) = (1.3)(0.6)(137,000 \text{ psi}) = 106,860 \text{ psi} \text{ (1.3 weak axis factor)}$$

$$F_b = M/S = (VL/2)/S \text{ (L/2 for guided bending)}$$

$$V = 2SF_b/L = (2)(0.000482 \text{ in}^3)(106,860 \text{ psi})/0.25" = 412 \text{ lb.}$$

Bearing of #8 Screw on Strap Anchor

$$V_a = 2.7DtF_{tu}/3.0$$

$$V_a = 2.7(0.164")(0.033")(45,000 \text{ psi})/3.0$$

$$V_a = 219 \text{ lb.}$$



Alternate Installation – Strap Anchor to Concrete (Continued)

Bearing of #8 Screw on Frame

$$V_a = F_e D t / K_D = (3,350 \text{ psi})(0.164")(0.75") / (10(0.164) + 0.5) = 193 \text{ lb}$$

Capacity of Connection is 181 lb (only one concrete screw per strap)



Alternate Installation – Strap Anchor to CMU

3/16" Tapcon Anchor; 2-1/2" Minimum Edge Distance, 1-1/4" Minimum Embedment

#8 Screws Connecting Strap to Frame

3/4" thick Wood Frame

20 gauge (0.033" thick) 33 KSI Steel Strap Anchor

1/4" Maximum Shim Space

Minimum ASTM C90 Concrete Masonry Unit

Allowable Shear of 3/16" Tapcon Anchor

$$P_{ss}/\Omega = 135 \text{ lb} \quad (\text{NOA 21-0201.06})$$

Bearing of 3/16" Tapcon Anchor on Strap Anchor

$$V_a = 2.7D_tF_{tu}/3.0$$

$$V_a = 2.7(0.170")(0.033")(45,000 \text{ psi})/3.0$$

$$V_a = 227 \text{ lb.}$$

Bending of 3/16" Tapcon Anchor

$$L = 1/4" \text{ (Maximum Shim Space)}$$

$$S = \pi d^3/32 = \pi(0.170")^3/32 = 0.000482 \text{ in}^3$$

$$F_b = (1.3)(0.6F_y) = (1.3)(0.6)(137,000 \text{ psi}) = 106,860 \text{ psi} \text{ (1.3 for weak axis bending)}$$

$$F_b = M/S = (VL/2)/S \text{ (L/2 for guided bending)}$$

$$V = 2SF_b/L = (2)(0.000482 \text{ in}^3)(106,860 \text{ psi})/0.25" = 412 \text{ lb.}$$

Bearing of #8 Screw on Strap Anchor

$$V_a = 2.7D_tF_{tu}/3.0$$

$$V_a = 2.7(0.164")(0.033")(45,000 \text{ psi})/3.0$$

$$V_a = 219 \text{ lb.}$$



Alternate Installation – Strap Anchor to CMU (Continued)

Bearing of #8 Screw on Frame

$$V_a = F_e D t / K_D = (3,350 \text{ psi})(0.164 \text{ in})(0.75 \text{ in}) / (10(0.164) + 0.5) = 193 \text{ lb}$$

Capacity of Connection is 135 lb (only one concrete screw per strap)



Alternate Installation – Strap Anchor to Wood – Cap Installation

Two #8 x 1-1/2" Flat Head Screws securing strap to substrate

Spruce-Pine-Fir 2x Wood Substrate Minimum (G=0.42)

Two #8 Screws securing strap to frame

3/4" thick Wood Frame

20 gauge (0.033" thick) 33 KSI Steel Strap Anchor

1/4" Maximum Shim Space

Allowable Withdrawal of #8 x 1-1/2" Flat Head Screw

$$W' = 1.6(82 \text{ lb/inch})(1.5") = 197 \text{ lb}$$

Allowable Pull-over of #8 x 1-1/2" Flat Head Screw

$$P_{\text{nov}}/\Omega = 1.5t_d F_u/\Omega = 1.5(0.033")(0.332")(45,000 \text{ psi})/3.0 = 247 \text{ lb}$$

Bearing of #8 Screw on Frame

$$V_a = F_e D t / K_D = (3,350 \text{ psi})(0.164")(0.75") / (10(0.164) + 0.5) = 193 \text{ lb}$$

Bearing of #8 Screw on Strap Anchor

$$V_a = 2.7 D t F_{tu} / 3.0$$

$$V_a = 2.7(0.164")(0.033")(45,000 \text{ psi}) / 3.0$$

$$V_a = 219 \text{ lb.}$$

Capacity of Connection is 193 lb

Capacity for Two Screws is 386 lb



72" x 79" XX Door +50/-55 psf

Anchorage Requirements

Through Frame validated by test.

Through Frame Capacity: 110 lb/anchor

Minimum Alternate Anchor Capacity: 122 lb/anchor

Minimum Alternate > As-Tested **Alternate Anchorages OK**



Appendix A

Revision Log

<u>Identification</u>	<u>Date</u>	<u>Page & Revision</u>
Original Issue	04/02/23	Not Applicable